

Effect of iron and nickel substitution on the piezoelectric properties of PZT type ceramics

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Abstract

The effect of Fe and Ni doping on piezoelectric properties of a soft type piezoelectric material was investigated. The materials composition was as follows: $\text{Pb}_{0.95}\text{Bi}_{0.03}\text{Nb}_{0.02}\text{Zr}_{0.51}\text{Ti}_{0.49-x}\text{M}_x\text{O}_3$, where M stands for the transitional metals Fe or Ni and $x=0; 0.02; 0.04; 0.06; 0.08; 0.10$. The materials were prepared by the conventional ceramic technique, using high purity oxides, mixed in a planetary ball mill for 3 hours and double calcined at 850 °C and 900 °C for 2 hours, with an intermediate milling of 4 hours and a final milling of 48 hours in order to get a final powder with crystallites in the nanometric range. X-ray diffractograms showed that compounds were completely formed and they were situated in the nanometric range with an average crystallite size of about 95 nm. The pressed and sintered samples of these materials showed maximum densification of about 98.5 % of TD at an optimum sintering temperature of 1200 °C for both types of materials. The optimum amounts of doping for both types of transitional elements were situated somewhere around $x=0.06$ with better results for nickel doped samples. Thus the maximum density for 0.06 nickel doped material was 7.87 g/cm³ while for iron doped one it was only 7.80 g/cm³. The piezoelectric properties followed consequently the same trend. Thus the electromechanical coupling factor k_p for 0.06 nickel doped samples was 0.665 while for the correspondingly iron doped ones it was 0.638. The relative dielectric constant was about 4050 for nickel doped samples and 3400 for iron doped ones. The corresponding values for the charge constant d_{33} were 625 pm/V and 530 pm/V respectively. These results were discussed in terms of the positions occupied by Ni and Fe into the lattice, the type of vacancies created by this and the shift of the morphotropic phase boundary.

Keywords: PZT; Perovskite; Piezoelectric properties; Dielectric properties; Sintering,

1. Introduction

At present there is an increasing demand for high quality piezoelectric materials used for the fabrication of the piezoelectric transducers for various applications in the field of sensors and actuators for fine displacement systems, especially in microrobotics or microelectromechanical systems.

Actuators make use of the direct expansion of piezoelectric materials and therefore for such applications there is a need for piezomaterials with high displacement constant d ¹⁻⁷. Moreover, during the last years another striking application of the reverse piezoelectric effect was developed in the field of micromotors⁸⁻¹¹, in large demand today as tiny motors for office equipment and microrobotics. Such piezoelectric micromotors are superior in the millimetric-size motor area to any other motors because their efficiency is completely insensitive to size. They can work with the same efficiency at low or high speed still retaining higher torque, have excellent controllability and fine position resolution. Do not require gear mechanism, are very quiet in operation and are not affected by the external magnetic and radioactive fields. Therefore, piezoelectric materials with large charge constant d for such applications become imperative and the present investigation was

conducted toward obtaining new PZT type materials with large d constant and still having high electromechanical coupling coefficient able to be used for actuators and micromotors sensors and transducers.

2. Experimental

The materials investigated in the present work were a soft type PZT material doped with nickel and iron and having the general chemical formula: $\text{Pb}_{0.95}\text{Bi}_{0.03}\text{Nb}_{0.02}\text{Zr}_{0.51}\text{Ti}_{0.49-x}\text{M}_x\text{O}_3$, where M stands for the transitional metal Ni or Fe and $0.00 \leq x \leq 0.10$. The raw materials used for the experiment were oxides of p.a. purity. The materials were processed by the conventional ceramic technique with the following detailed data: six charges of each dopant Ni and Fe were prepared, corresponding to $x=0.00; 0.02; 0.04; 0.06; 0.08$ and 0.10 respectively. The stoichiometric amounts of oxides were wet mixed for 3 h by means of a planetary ball mill, in agate vials of 500 ml capacity, using agate balls of about 10 mm diameter in a weight ratio: ball/oxides/acetone of 100/100/250. The mixed slurries were dried with continuous agitation on electrical plates, manually crushed and sieved and then double calcined at 850 °C and 950 °C respectively for 2 h with an intermediate milling of 4 h and a final milling of 48 hours. BET measurements of the final milled

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powders gave an average specific surface area between 10-12 m²/g corresponding to an average particle diameter of about 90-100nm. Disc shaped samples of 15 mm diameter and about 2 mm thick were next uniaxially pressed from these powders in a steel die at a pressure of about 50 MPa. The pressed samples were then sintered in dense alumina crucibles at temperatures between 1050 and 1300 °C for 4 h. The density of each sintered sample was determined by Archimede's method. Next, the sintered samples were processed by grinding on a mechanically grinding machine up to a final dimension of 10 mm diameter and 1 mm thick. After ultrasonically cleaning and thermally recovery at 700 °C for 1 h, the samples were silver electroded on both plan parallel surfaces and poled in a silicon oil bath at 220 °C under an electric field of 30 KV/cm and slowly cooled down to 80 °C under electric field after which the electric field was cut off and the samples taken out from the poling device. Piezoelectric properties were measured 24 h after poling by resonance spectroscopy using a HP 4194A Impedance gain/phase analyzer.

3. Results and discussion

Fig. 1 shows an example of the X-ray spectrum of a Ni doped calcined powder. As can be seen the PZT phase with perovskite structure is well formed, indicating that the PZT material synthesis was completely achieved. X-ray diffractograms were made for all powders investigated, but they are not shown here because they were entirely similar to this one.

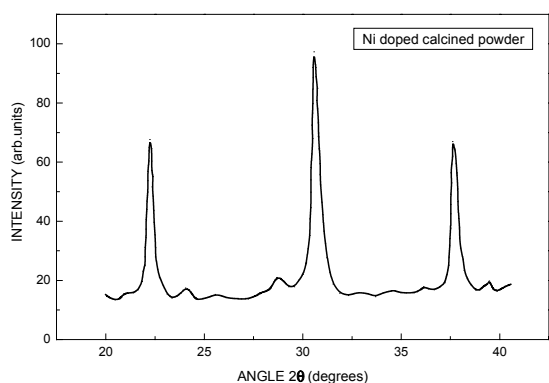


Fig. 1 X-ray diffractogram of the 0.06 Ni doped calcined powder sample

Figures 2 and 3 illustrate the behavior of the densities of sintered samples as a function of the sintering temperature for all composition doped with Ni (fig. 2) and Fe (fig. 3) respectively.

One can see that for both types of composition there is an optimum sintering temperature centered on 1200

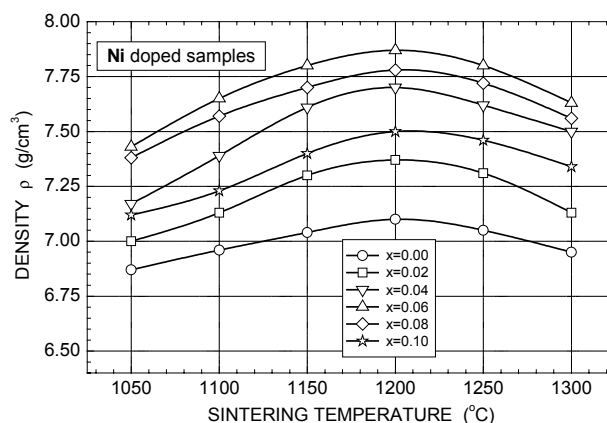


Fig. 2 The dependence of the density on the sintering temperature for Ni doped samples

°C where the densities reach a maximum regardless the amount of dopant. With increasing the dopant amount x the densities increase, reaching the highest values for compositions with $x=0.06$ and then decreasing again.

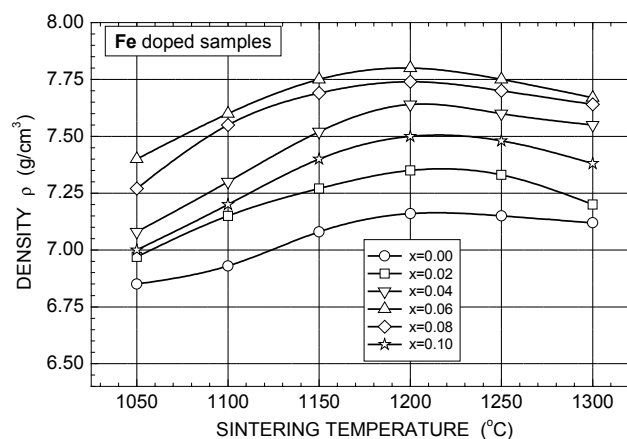


Fig. 3 The dependence of the 0.06 Fe doped calcined powder sample

This behavior is well illustrated in the graph from fig. 4 where one can see the maximum densities of 7.87 g/cm³ and 7.80 g/cm³ for the Ni and Fe doped samples respectively, values which correspond to about 98.5 and 97.5 % respectively of the theoretical density (if 8 g/cm³ is taken as the right figure for the theoretical density of a PZT material¹²). These values would be even slightly higher if the theoretical density should be considered as 7.95 g/cm³¹³ or 7.98 g/cm³¹⁴.

Such high values for the densities indicate that the sintered samples are fully densified with well-formed crystallites and rather poreless. This assertion is fully sustained by the fracture SEM images from fig. 5 made on 0.06 Ni and 0.06 Fe doped samples with the highest densities.

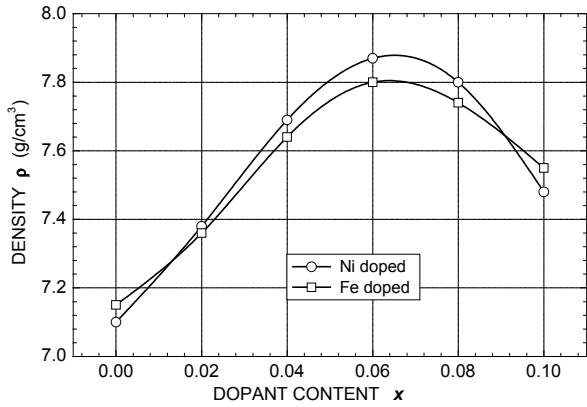
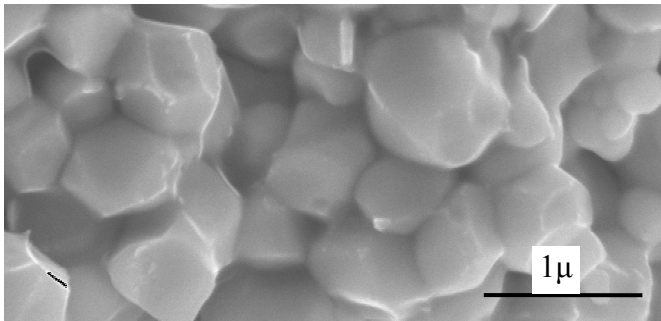
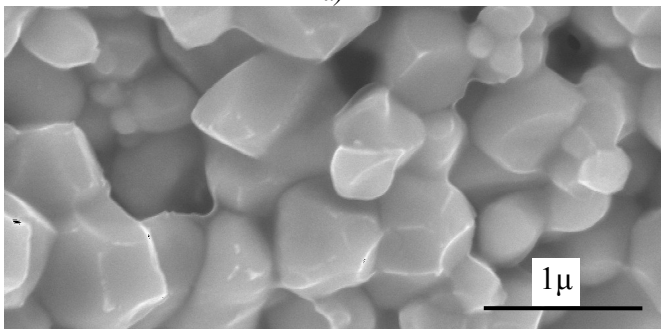


Fig. 4 The behavior of the maxim values of the density as a function of the dopant amount for Ni and Fe doped samples, sintered at 1200 °C



a)



b)

Fig. 5 Fracture SEM images of the sintered samples doped with 0.06 Ni (a) and 0.06 Fe (b) respectively

One can see the lack of pores, and the well formed submicronic crystallites. One may expect the best piezoelectric properties for these samples as will be confirmed further.

The decrease of the densities for samples with $x > 0.06$ could possible be explained by a slight inhibiting effect of the dopants for higher concentrations. Fig. 6 shows a micrograph of a Fe doped sintered sample with $x = 0.10$ where the crystallites are smaller and some pores are present. The piezoelectric properties were determined only on samples with maximum densities, i.e. the samples sintered at 1200 °C.

One can see that k_p reaches maximum values of 0.665

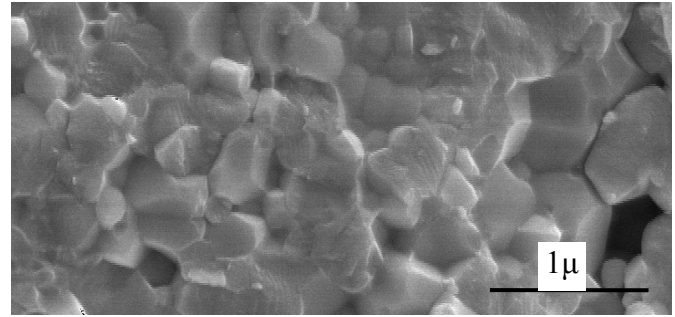


Fig. 6 Fracture SEM image of a sample doped with 0.10 Fe

Fig. 7 shows the dependence of the planar coupling coefficient k_p on the dopant concentration.

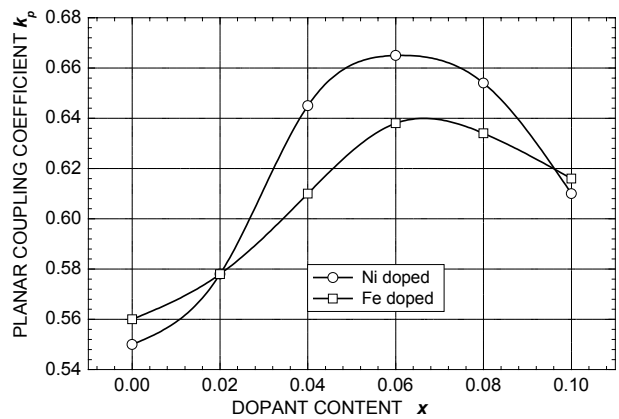


Fig. 7 The dependence of the planar coupling factors of Ni and Fe doped samples on the dopant concentration

and 0.638 for the compositions with $x = 0.06$ both for Ni and Fe doped samples respectively. The same trends and behaviors were recorded for charge constant d_{33} and dielectric permittivity ϵ_r either as shown in fig 8 and 9.

A remarkable thing about these graphs is the high values of the constants mentioned before. Thus, for Ni doped samples, a maxim value of about 625 pm/V for d_{33} was measured and 530 pm/V for Fe doped samples respectively. Such values can be considered very high for an ordinary doped PZT material and this fact makes such materials excellent candidates for actuators or micromotors.

At the same time the dielectric permittivities at room temperature reach also high values of nearly 4050 and 3400 for Ni and Fe doped samples respectively. This might be the result of a slight decrease of the Curie temperature. In fact all these experimental results can be explained by the assumption that the presence of the dopants gives rise to A vacancies into the PZT lattice with the direct consequence of rising the dielectric constant, the piezoelectric coupling factor and the charge constant¹⁵. This is consistent with the ionic

radius rule. Thus Ni^{2+} has an ionic radius of 0.69 Å and enters the Ti^{4+} position which has a radius of 0.68 Å.

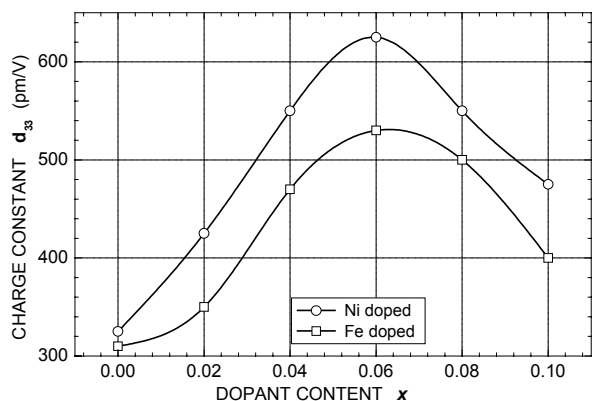


Fig. 8 The dependence of the charge constant d_{33} of Ni and Fe doped samples on the dopant concentration

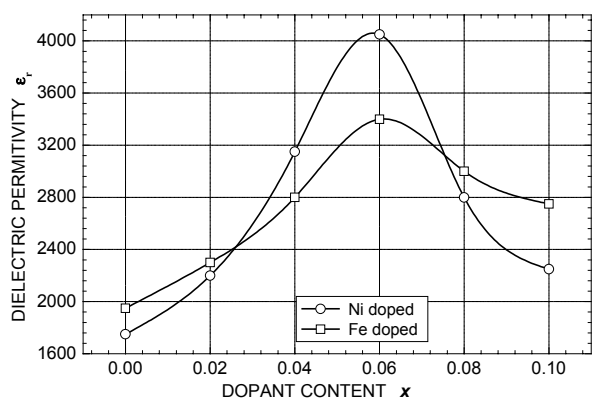


Fig. 9 The dependence of the relative dielectric permittivity of Ni and Fe doped samples on the dopant concentration

On the other hand Fe^{2+} with its 0.75 Å ionic radius, most probably enters Zr^{4+} position with 0.80 Å ionic radius. Thus the tetragonal and the rhombohedral phases are equally affected by the presence of Ni and Fe and forms a new morphotropic phase boundary probably at $x = 0.06$ ¹⁶, where the piezoelectric properties are subsequently enhanced because of the increased easy of reorientation during poling¹⁷. A shift of R and T phases is also possible by the new distribution of Ni and Fe ions into the lattice. Such a shift forms stronger piezoelectric effects by the easiness of domain reorientation. Within the R side the number of 180° domains is greater and they are more easily aligned along the poling field direction than the 90° domains which switch harder. In thus way it seems easy to assume a higher degree of alignment of dipoles after removal of the field and consequently higher piezoelectric parameters for the Ni doped compositions.

4. Summary

A soft type PZT material was doped with nickel and iron within a narrow compositional range. The materials were prepared by the conventional ceramic technique and were sintered at temperatures up to 1300 °C. The optimum sintering temperature proved to be 1200 °C for both types of doped samples. The samples sintered at this temperature and having a doping level of 6 % atomic, gave the highest piezoelectric parameters: densities of 7.87 and 7.8 g/cm³, electromechanical coupling factors of 0.665 and 0.638, dielectric permittivities of 4050 and 3400 and charge constants of 6.25 and 5.30 pm/V for Ni and Fe samples respectively. The Ni doped samples were better than Fe doped ones.

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